

Joint Summer School on Fuel Cell and Hydrogen Technology
21-25 August 2011, Viterbo, Italy

Hydrogen fires tutorial

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Purpose of this tutorial

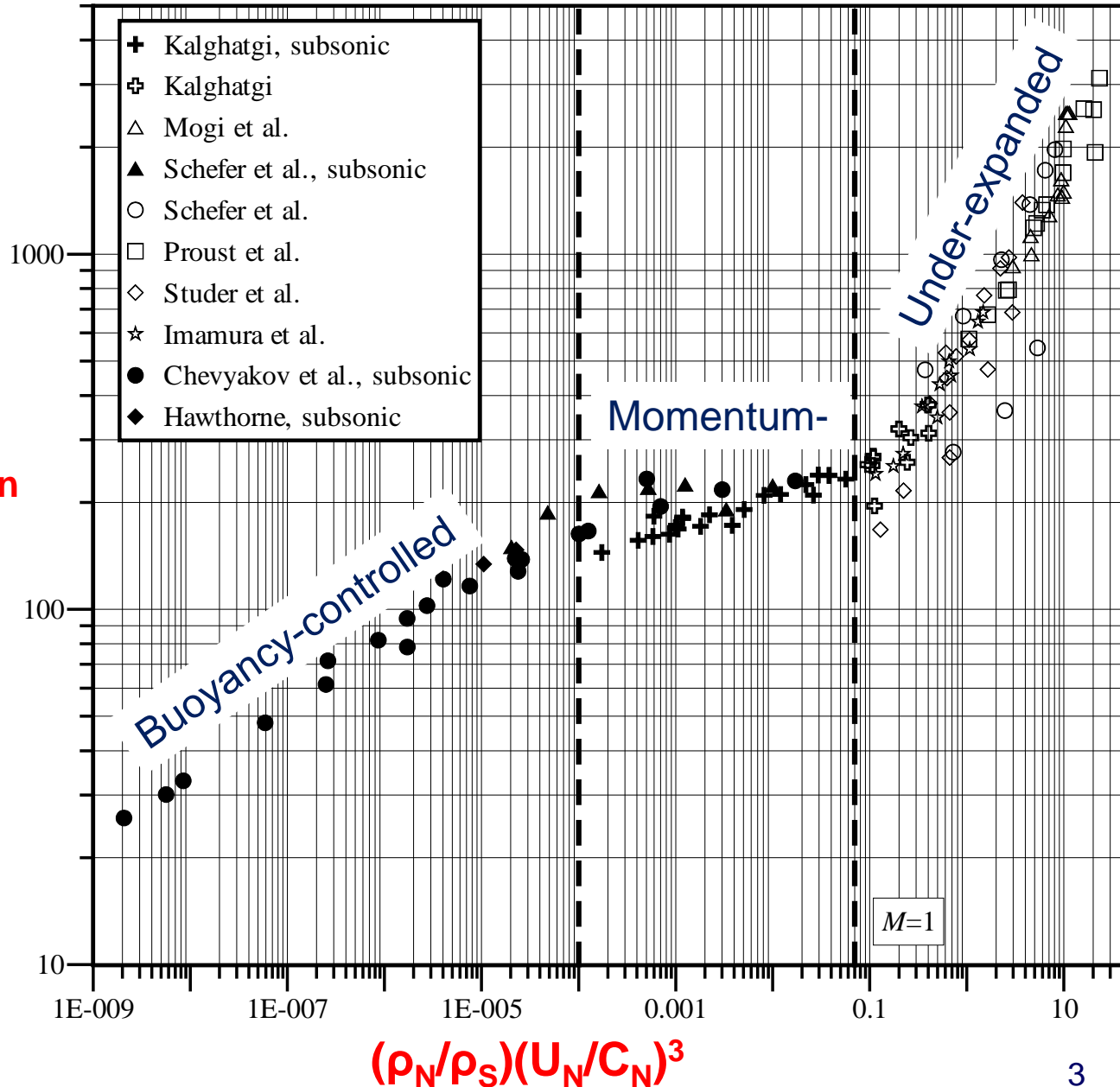
- ❖ Assist with coursework!
- ❖ Give “ball park” figures for realistic examples
- ❖ Build on unignited jets covered yesterday – compare flammable envelope with flame length for the same scenario
- ❖ Focus on jet fires – specifically flame length

The dimensionless correlation

Validation:
 $P=0.1-90$ MPa
 $d=0.4-51.7$ mm

Line $M=1$
(choked flow)

L_f/d_n
 L



The dimensionless correlation

- ❖ Y axis: L_f/d_n where L_f = flame length, d_n = nozzle diameter
- ❖ X axis: $(\rho_N/\rho_S)(U_N/C_N)^3$ where
- ❖ ρ_N = density at the nozzle exit,
find the same way as with similarity law for unignited jets
equal to 0.0838 kg/m^3 at normal temperature and pressure (NTP) for sub-sonic and expanded sonic jets

IF the jet is underexpanded then the density is calculated by an **under-expanded jet theory** developed at the University of Ulster

- ❖ ρ_S = density of the surroundings = 1.205 kg/m^3 for air
- ❖ C_N = is the speed of sound in hydrogen at the nozzle exit,

$$C = \sqrt{\gamma \frac{P}{\rho}} = \sqrt{\gamma \frac{RT}{M}}$$

- ❖ U_N = the velocity of the hydrogen at the jet exit
 $U_N = C_N$ for sonic and supersonic jets,
for subsonic jets:

$$U_N = \sqrt{2 \frac{\Delta P}{\rho}}$$

Example: 200 bar, 1mm orifice

- ❖ Take storage temperature = 288 K
- ❖ $\rho_N = 9.287 \text{ kg/m}^3$ (underexpanded jet theory- pressure ratio >1.9 bar)
- ❖ $\rho_s =$ density of the surroundings, 1.205 kg/m^3 for air
- ❖ $d_n =$ diameter = 0.001 (make sure in m, SI units)
- ❖ Yesterday we found the distance to the LFL

$$C_{ax}^m = 5.4 \sqrt{\frac{\rho_N}{\rho_s} \frac{D}{x}} \quad x = 5.4 \sqrt{\frac{\rho_N}{\rho_s} \frac{D}{C_{ax}^m}} \quad x = \underline{5.20 \text{ m}}$$

How does the flame length compare??

Y axis: L_f/d_n we know d_n , we need to find L_f

X axis: $(\rho_N/\rho_s)(U_N/C_N)^3$ $\rho_N = 9.287 \text{ kg/m}^3$ as above,
 $\rho_s = 1.205 \text{ kg/m}^3$ for air

jet is underexpanded so we don't need to calculate U_N and C_N

5 Therefore x axis = $(9.287/1.205)*1 = 7.707$

Example: 200 bar, 1mm orifice

x axis = 7.707

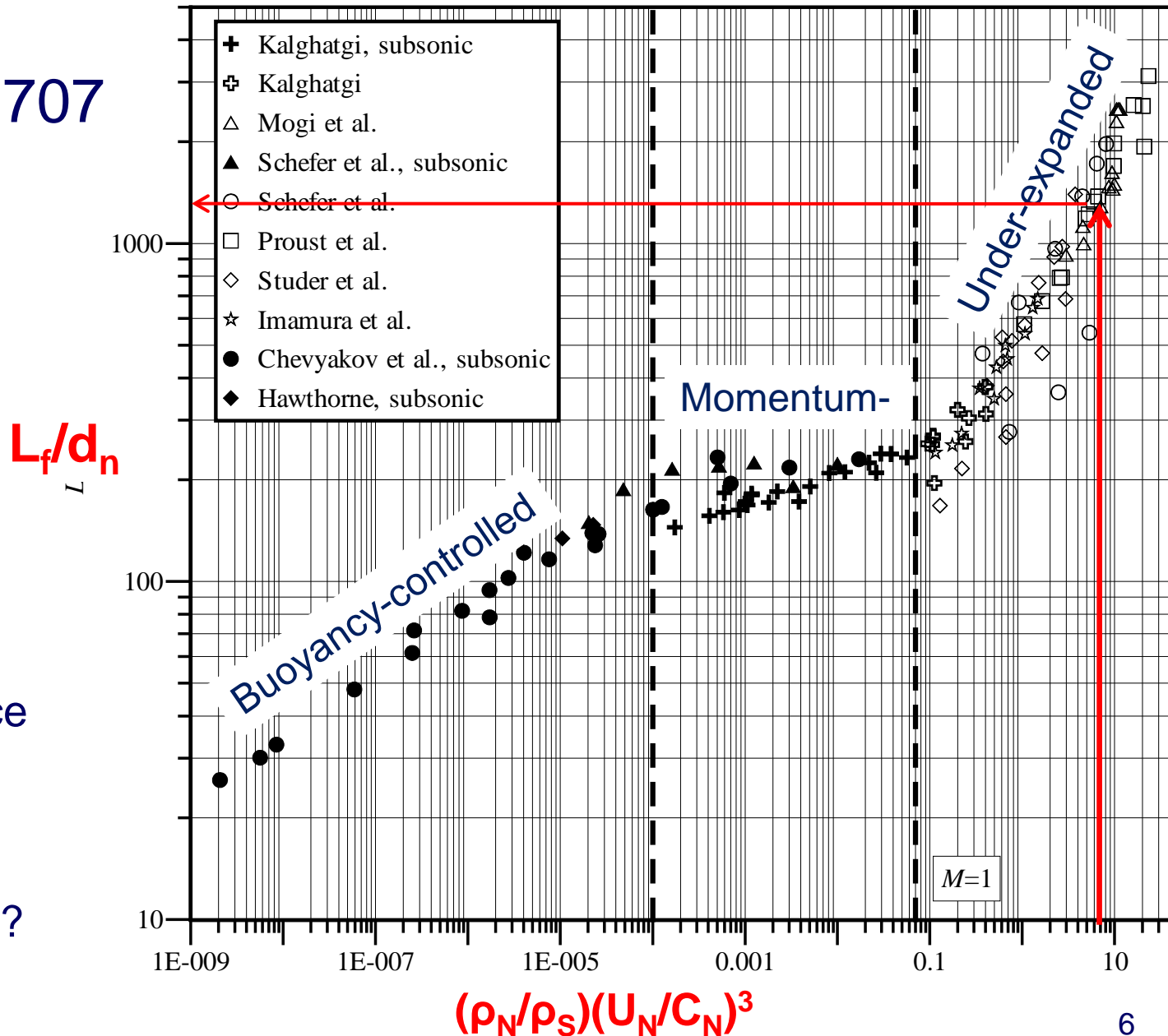
y axis ~ 1500

$L_f/d_n \sim 1500$

For 1mm
Flame length is in
region of 1.5m

Remember distance
to 4% was 5.2 m

What about a
diameter of 5 mm??



Example: 200 bar, 1mm orifice, 3mm pipe

- ❖ Same case as previous, but now short length of 3mm diameter pipe after the 1mm orifice (i.e. like 1mm pipe restrictor)
- ❖ Note the jet is still underexpanded
- ❖ Assume no losses as jet expands and no drop in temperature
- ❖ Will the addition of a pipe affect the flame length???

How does the flame length compare??

Y axis: L_f/d_n we know d_n , (now 3mm) we need to find L_f

X axis: $(\rho_N/\rho_S)(U_N/C_N)^3$ $\rho_S = 1.205 \text{ kg/m}^3$ for air
As before $U_N = C_N$

$\rho_N = \text{?????}$

Mass flow rate is conserved in the pipe

Example: 200 bar, 1mm orifice, 3mm pipe

- ❖ Mass flow rate is conserved in the pipe
- ❖ Mass flow rate = ρVA
- ❖ $\rho_{1\text{mm}} V_{1\text{mm}} A_{1\text{mm}} = \rho_{3\text{mm}} V_{3\text{mm}} A_{3\text{mm}}$
- ❖ Velocity is the speed of sound, the same in each case
- ❖ We know area because we know diameter $A = \pi d^2/4$
- ❖ $\rho_{3\text{mm}} = \rho_{1\text{mm}} A_{1\text{mm}}/A_{3\text{mm}} = 9.287 * (\pi(0.001)^2/4)/(\pi(0.003)^2/4)$
- ❖ $\rho_{3\text{mm}} = 1.03 \text{ kg/m}^3$
- ❖ Therefore x axis = $(1.03/1.205)*1 = 0.856$

Example: 200 bar, 1mm orifice, 3mm pipe

x axis = 0.856

y axis ~ 420

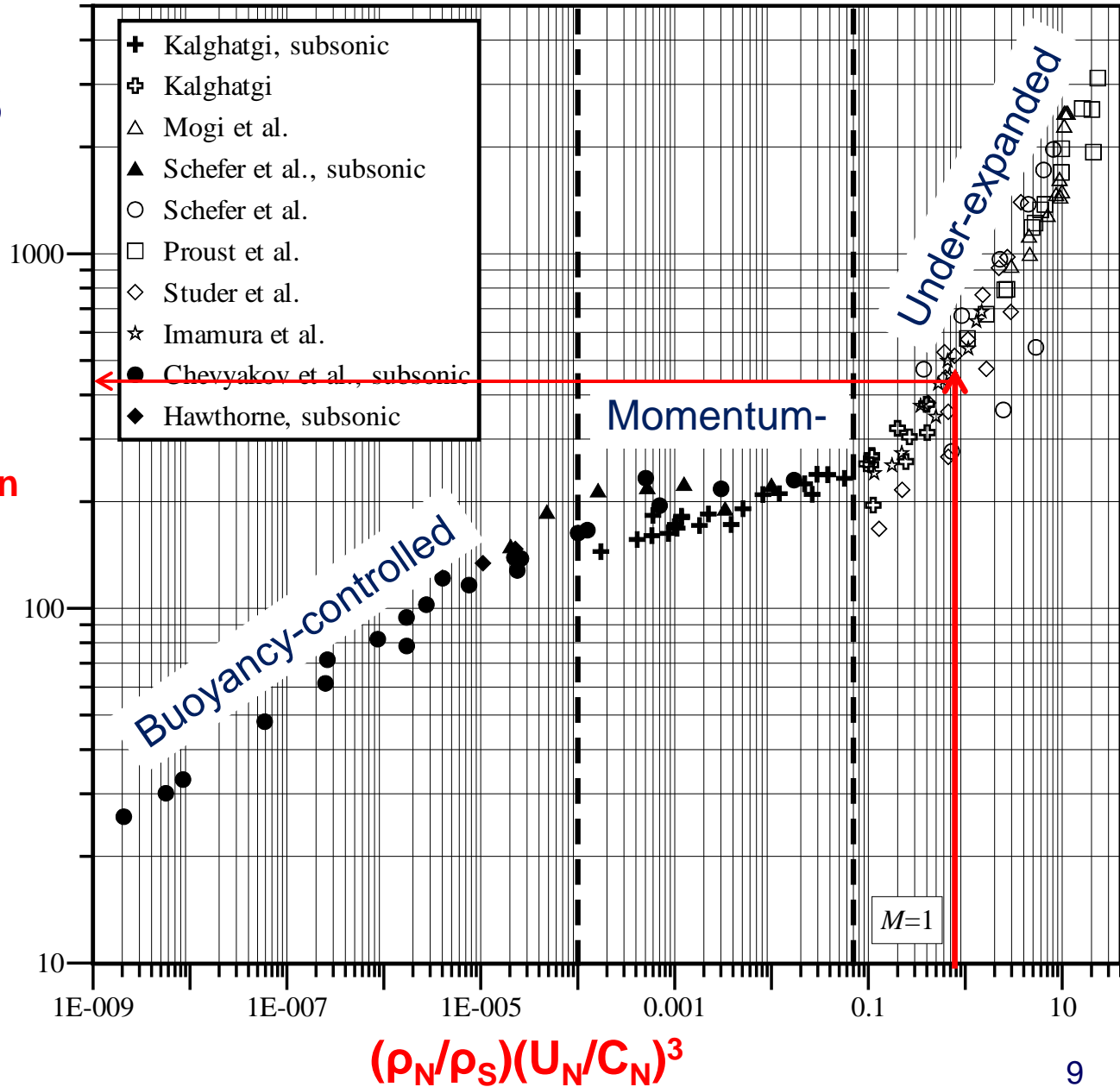
$L_f/d_n \sim 420$

L_f/d_n

Remember for 1mm Diameter, no pipe
 L_f = region of 1.5m

Now with 3mm pipe

Slightly reduced =
 $420 \cdot 0.003 = 1.26 \text{ m}$



Example: 1.4 bar, 1mm orifice

- ❖ Take storage temperature = 288 K
- ❖ $\rho_N = 0.0838 \text{ kg/m}^3$ (pressure ratio <1.9 bar)
- ❖ $\rho_s =$ density of the surroundings, 1.205 kg/m^3 for air
- ❖ $d_n =$ diameter = 0.001 m

Y axis: L_f/d_n we know d_n , we need to find L_f

X axis: $(\rho_N/\rho_s)(U_N/C_N)^3$ $\rho_N = 0.0838 \text{ kg/m}^3$ as above,
 $\rho_s = 1.205 \text{ kg/m}^3$ for air

We need to calculate U_N and C_N

$$C_N = \sqrt{\gamma \frac{RT}{M}} = \sqrt{1.4 \frac{288 * 8314}{2}} = 1295 \text{ m/s} \quad U_N = \sqrt{2 \frac{\Delta P}{\rho}} = \sqrt{2 \frac{40000}{0.0838}} = 977 \text{ m/s}$$

$$\text{X axis} = (0.0838/1.205)(977/1295)^3 = 0.03$$

Example: 1.4 bar, 1mm orifice

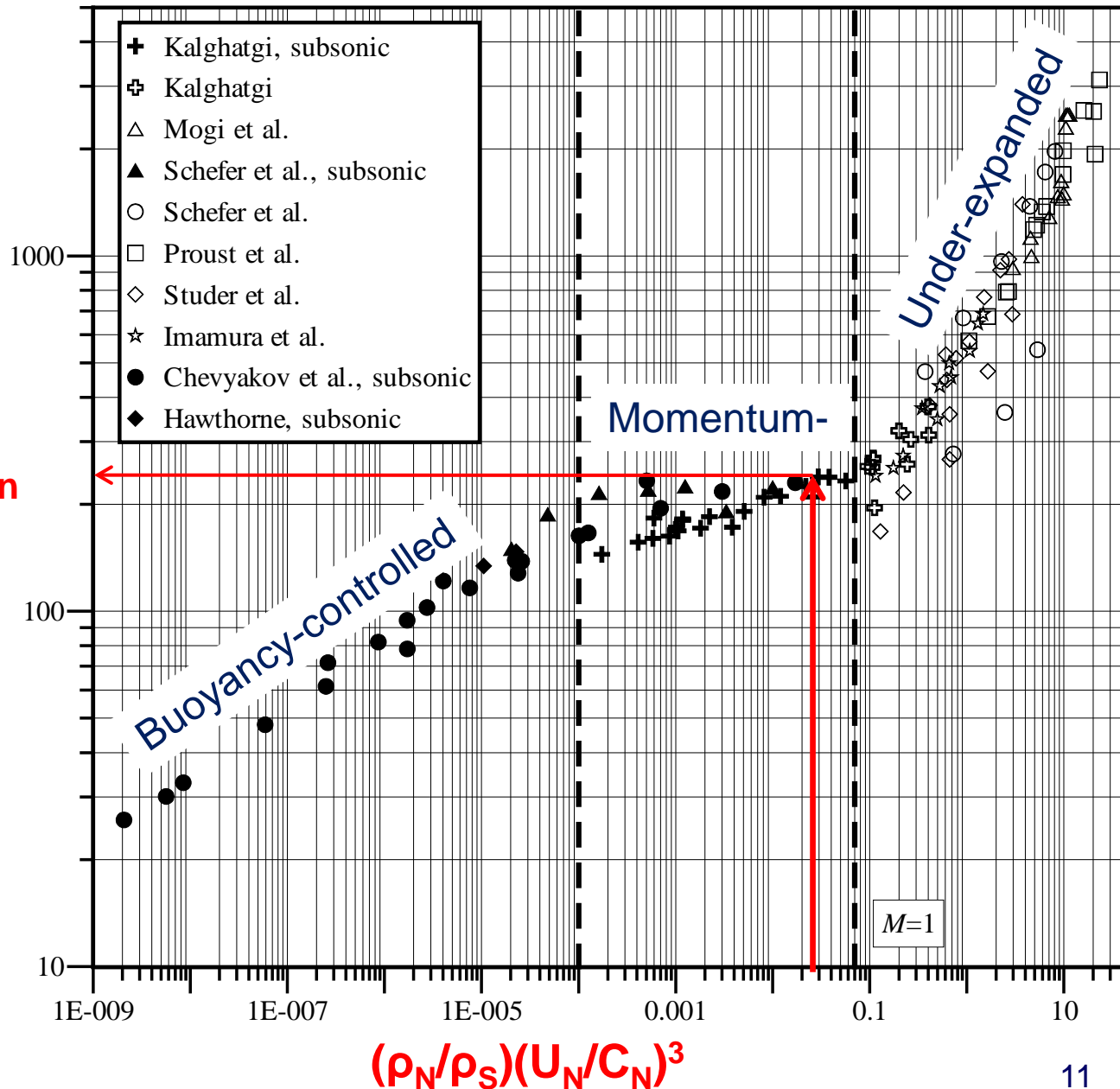
x axis = 0.03

y axis ~ 250

$L_f/d_n \sim 250$

Flame length = 0.25m

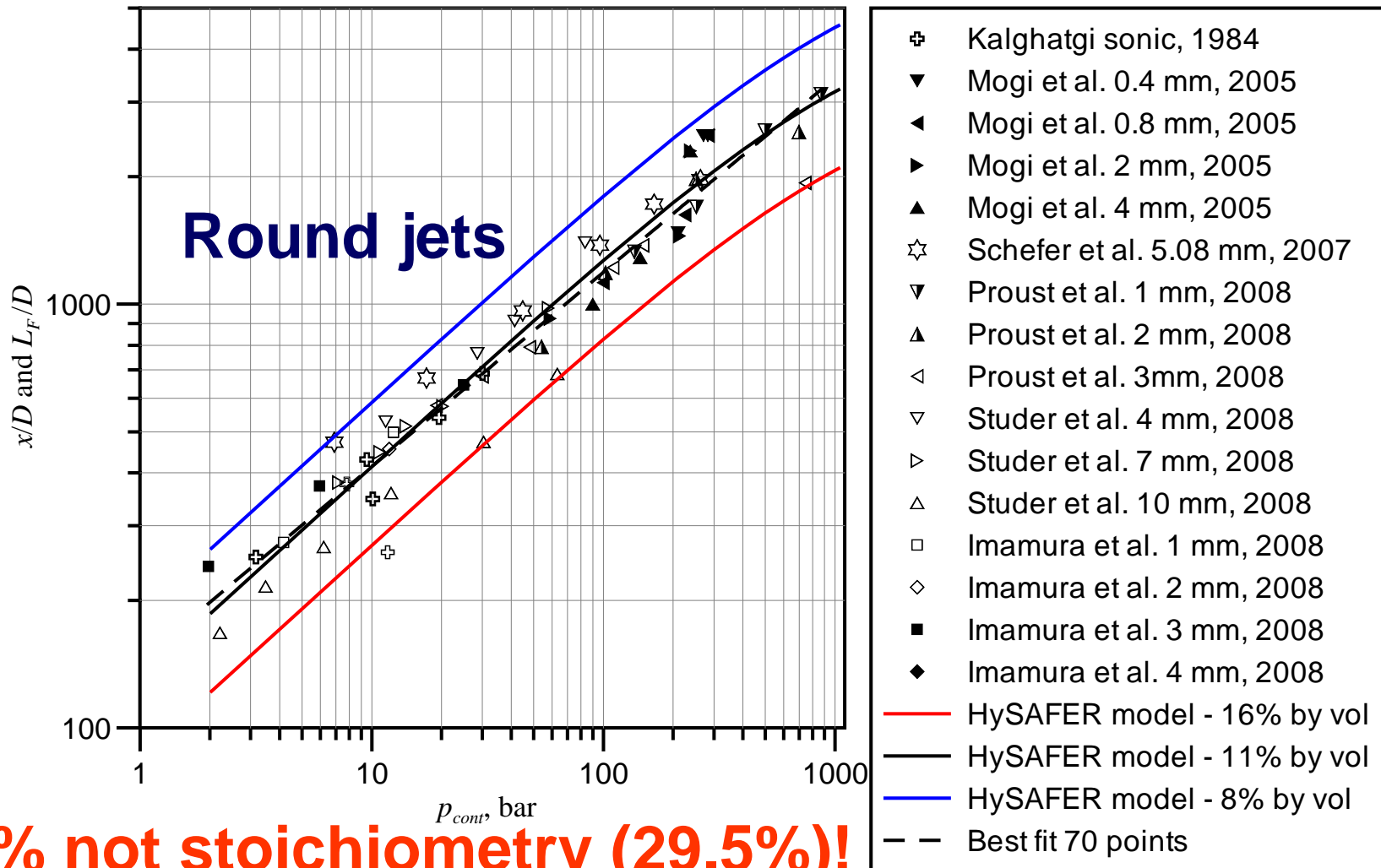
L_f/d_n



Separation distance – one language

❖ Flammable envelope – 4% by volume (LFL)

❖ Jet flame tip location – 11% in unignited jet (8-16%)



Any questions?

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